

## Control of Chaos in a Current Mode Controlled Buck Boost Converter Using Weak Periodic Perturbation Method

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### ABSTRACT

This paper analyses the nonlinear phenomena in current mode controlled buck-boost converter. The system undergoes various operating regions whenever there is a change in non linear elements presented in the system as well as in the loads. In this work, inductor current is considered as the reference for analysis. The results show that the converter enters into period-1, periodic doubling and chaotic regions as per the parameter ( $I_L$ ) variations. The proposed control strategy, weak periodic perturbation (WPP) method tries to stabilize the system from the chaotic behavior. The buck boost converter along with the control system is simulated using MATLAB/SIMULINK software tool and the results are presented. The hardware implementation of the system is done and the results are verified with the simulation results. It shows that the WPP can transform the system behaviour from the chaotic region to the periodic one.

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## 1. INTRODUCTION

The power electronic dc-dc converters are the most non-linear and time varying systems. Since these topologies have active switches, passive elements and power diodes with nonlinear voltage, current characteristics, they are dynamic in nature [1]. The operating modes of switching converters are turning into chaotic very easily [2-4]. A dc-dc buck-boost converter with current mode controlled in continuous conduction mode gives rise to a great variety of behaviour depending on the parameters of the circuits. The behaviour of the buck boost converter is analysed with inductor current as the bifurcation parameter [5]. The converter enters into period-1 to the chaotic regime as the inductor current varies. So it is very essential to implement a control strategy to avoid chaos. There are many control strategies are available in the literature. There are two different categories, namely feedback and non feedback control methods. Ott-Grebogi-Yorke (OGY) and Time-delayed frequency control, etc are few of the control methods falling under feedback control strategies [6-7]. In feedback methods, anyone of the system variable is taken and the control law is implemented to attain the objective. In non feedback method, system variables need not to be measured. Any one of the periodic orbit need to be identified as the control target. This paper investigates current mode controlled buck boost converter with weak periodic perturbation method [8]. Simply, by adding a weak sinusoidal external force to the original system, narrow and high sub harmonic steps are stabilized.

## 2. ANALYSIS OF BUCK BOOST CONVERTER

The buck-boost converter provides the output voltage either greater or lesser than the available voltage based on the duty ratio. It has low cost, high efficiency, and low noise. Buck-boost converters are used in automobiles, consumer goods and various applications. A buck-boost converter consists of an active switch S, a powerful diode D, energy storing elements (one inductor L and one capacitor C) with a load resistor  $R_L$ . Current mode control strategy is applied in this analysis. The converter is operated with the duty ratio of D and with the switching frequency of f. The average output voltage of the converter is given by,

$$V_0 = -\left(\frac{D}{1-D}\right) * V_{in} \quad (1)$$

Where,  $V_{in}$  = input voltage

The average load current is

$$I_{out} = \frac{V_0}{R_L} \quad (2)$$

The source current is,

$$I_s = \frac{I_0 * V_0}{V_{in}} \quad (3)$$

The average inductor current is,

$$I_{Lavg} = \frac{I_s}{D} \quad (4)$$

Peak-peak ripple current is,

$$\Delta I_L = \left(\frac{V_{in}}{L}\right) * DT \quad (5)$$

Where, T is the switching time period

The minimum value of the inductor for continuous conduction mode is,

$$I_{min} = \left(\frac{R}{2f}\right) * (1-D)^2 * H \quad (6)$$

The capacitor ripple is expressed as

$$\frac{\Delta V_0}{V_0} = \frac{D}{Rcf} \quad (7)$$

Figure 1 shows the buck-boost converter operating in the continuous conduction mode. Two modes of operations are obtained by controlling the power switch S.

### 2.1. Mode 1 operation of the buck-boost converter

During this mode, diode D is reverse biased when switch S is gated ON. The inductor current rises up linearly from  $I_1$  to  $I_2$ . This mode is shown in Figure 2. The load current is delivered by the output capacitor C. The capacitor is designed in such a way that it can supply entire current to the load.

## 2.2. Mode 2 operation of the buck-boost converter

During this mode the switch is OFF at  $t=t_n$ . The inductor current decreases linearly from  $I_2$  to  $I_1$ . Figure 3 shows the mode 2 operation of the converter. It is not possible to have a sudden change in inductor current. So the voltage polarity in the inductor gets reversed to maintain the current constant. The inductor current decreases till the switch  $S$  is gated again. The energy stored in the inductor is delivered to the output capacitor  $C$ . This stored energy in the capacitor is drained out through the load when the switch is ON.

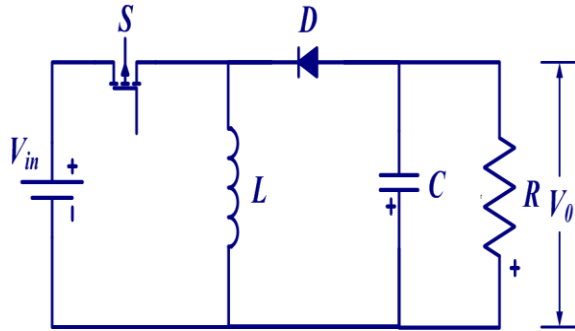


Figure 1. Circuit diagram of buck-boost converter

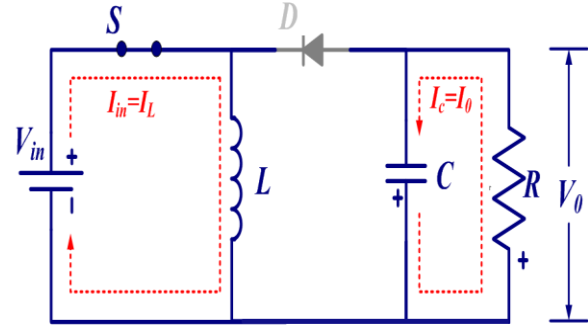


Figure 2. Equivalent circuit for the buck-boost converter during turn ON

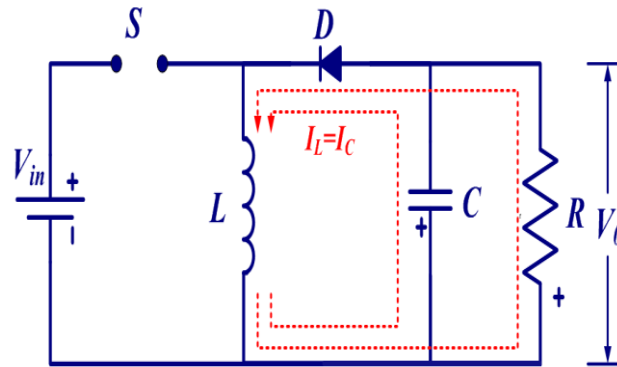


Figure 3. Equivalent circuit of the buck-boost converter during turn OFF.

## 3. OPERATION OF CURRENT PROGRAMMED BUCK-BOOST CONVERTER

The inner loop current controls are usually used for the buck-boost converters since the voltage-mode control will lead to instability. Also the converter experience right hand side zeroes in voltage mode control method [5]. The switch  $S$  is controlled by a feedback path that consists of a flip-flop and a comparator. The comparator compares the inductor current  $I_L$  and a reference current  $I_{ref}$ . The power switch is gated ON when the clock pulse is received and is triggered to OFF when the inductor current reaches  $I_{ref}$ . Figure 4 shows the current-mode controlled buck-boost converter. The inductance value and switching period  $T$  are chosen to operate the converter in continuous conduction mode. The switch  $S$  is closed at  $t=nt$ . The inductor current ramps linearly till  $I=I_{ref}$ . When  $I=I_{ref}$ , the comparator is triggered ( $Q=0$ ). Then it resets the clock pulse and triggers  $S$  to close again. The inductor current and capacitor voltage are shown in Figure 5. When switch  $S$  is closed, diode  $D$  is reversed biased. The steady state equations of the inductor current and the capacitor voltage during mode-1 are given by:

$$\frac{di}{dt} = \frac{E}{L} \quad (8)$$

$$\frac{dV_c}{dt} = -\left(\frac{1}{RC}\right)V_c \quad (9)$$

The current  $I$  ramps linearly during this period. As soon as the inductor current  $I$  attains the reference current  $I_{ref}$ , the switch is OFF. This method is known as peak-current-mode control. When switch  $S$  is off, diode  $D$  is ON. The steady state equations of the inductor current and the capacitor voltage during mode-2 are given by:

$$\frac{di}{dt} = -\left(\frac{1}{L}\right)V_c \quad (10)$$

$$\frac{dV_c}{dt} = -\left(\frac{1}{C}\right)\frac{V_c}{RC} \quad (11)$$

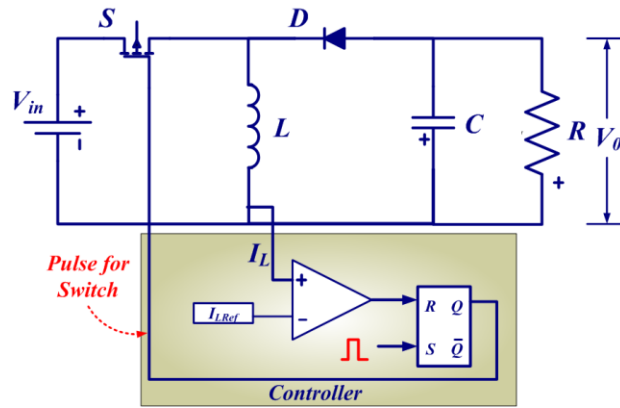


Figure 4. Circuit schematic of the current-mode controlled buck-boost converter

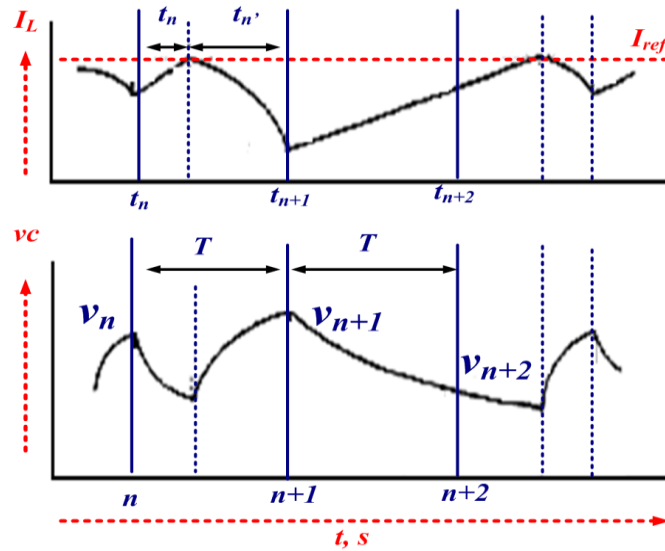


Figure 5. Typical waveforms of capacitor voltage & inductor current during turn off.

### 3.1 State equations of the converter

The state Equations of a buck-boost converter operated in continuous conduction mode is given by:

$$\frac{dx}{dt} = A_1 x + B_1 E, \quad nT \leq t \leq (n+1)T \quad (12)$$

$$\frac{dx}{dt} = A_2 x + B_2 E, (n+d)T \leq t \leq (n+1)T \quad (13)$$

Where, n=integer, T=Period, D=duty cycle,  $x = [V_c, i]^T$ , i=inductor current.  
When switch S is on, A and B is given by,

$$A_1 = \begin{bmatrix} \frac{-1}{C_1 R_1} & 0 \\ 0 & \frac{-R_2}{L_1} \end{bmatrix}, B_1 = \begin{bmatrix} 0 \\ \frac{1}{L_1} \end{bmatrix}$$

When switch S is OFF,

$$A_2 = \begin{bmatrix} \frac{-1}{C_1 R_1} & \frac{-1}{C_1} \\ \frac{1}{L_1} & \frac{-R_2}{L_1} \end{bmatrix}, B_2 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

#### 4. ROUTE TO CHAOS BY VARIING $I_{REF}$

The current programmed buck-boost converter is analysed under various operating regions. The reference current of the control method is increased for large values of  $I_{ref}$  and the system behaviour is analysed by simulation. The buck-boost converter model is simulated with the following design specifications articulated in Table 1. The system behaviour from period-1 to chaotic stage is analysed by varying the reference current in the range of 2.65A to 3A. The system is periodic in nature till the reference current reaches 2.65A. When the reference current is greater than 2.65A, the system will become more chaotic.

Tabel 1. Specification Parameter

Sr. No.	Parameter	Value
1	Input voltage	12V
2	Output voltage	18V
3	Inductor	1mH
4	Capacitor	4 uF
5	Load resistance	20 $\Omega$
6	Frequency (f)	20 kHz
7	Duty cycle (D)	0.6

##### 4.1. Period 1 Operation

It is desirable to operate the system in a fundamental regime which is the stable region of the system. By keeping the reference current  $I_{ref}$  at 2.65A, the period-1 operation is obtained. Figure 6 Shows the inductor current and output voltage waveform of the period-1 operation which is free from sub harmonics. The phase portrait of period-1 regime is shown in Figure 7.

##### 4.2. Period 1 Operation

When the bifurcation parameter  $I_{ref}$  is further increased to 2.85A, the period doubling stage is reached. This stage of operation is mostly avoided by design engineers. The inductor current and load voltage waveforms for the period-2 regime is shown in the Figure 10 and the corresponding phase portrait is shown in Figure 9.

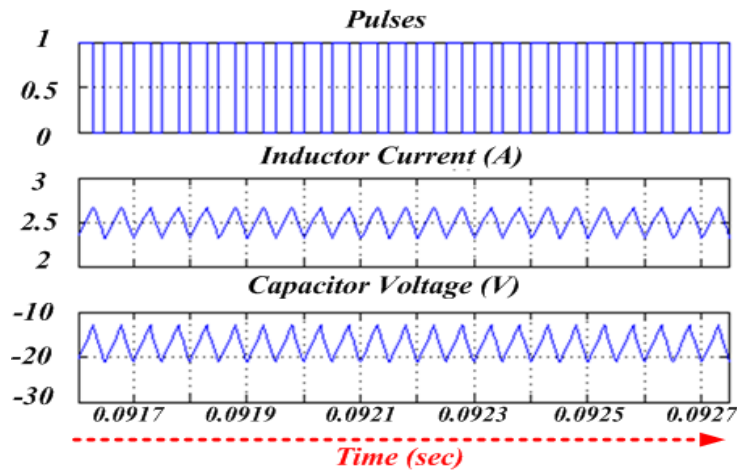


Figure 6. Waveforms of inductor current and capacitor voltage with  $i_{ref} = 2.65A$

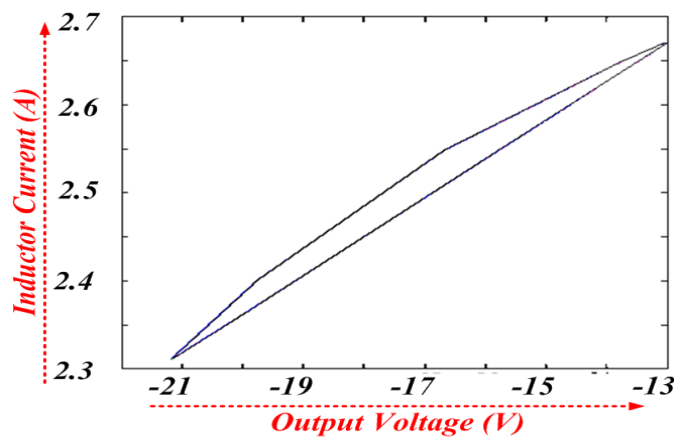


Figure 7. Phase portrait of period -1 regime

#### 4.3. Chaotic Operation

The chaotic regime is obtained when the value of reference current  $I_{ref}$  is increased to 3A. The simulated waveforms of inductor current and output voltage during chaotic operation are shown in the Figure 10 and the corresponding phase portrait is shown in Figure 11.

#### 4.4. Bifurcation diagram

Bifurcation diagram can be obtained varying any one of the system parameters, keeping all other parameters fixed [9]. The bifurcating parameters can be sourced voltage, capacitor voltage, inductor current, load resistance, inductance, and capacitance or clock frequency. The bifurcating diagram shown in Figure 12. is obtained by varying the inductor current. If the system is periodic all the points will lie on the same position. During the chaotic regime, all the points will be scattered and none of the dots will fall on the same position. Bifurcation diagram is drawn between capacitor voltage and reference current. From the Figure 9 it is understood that when the reference current is 2.85A, it bifurcates and when the reference current is 3A it enters into chaotic region.

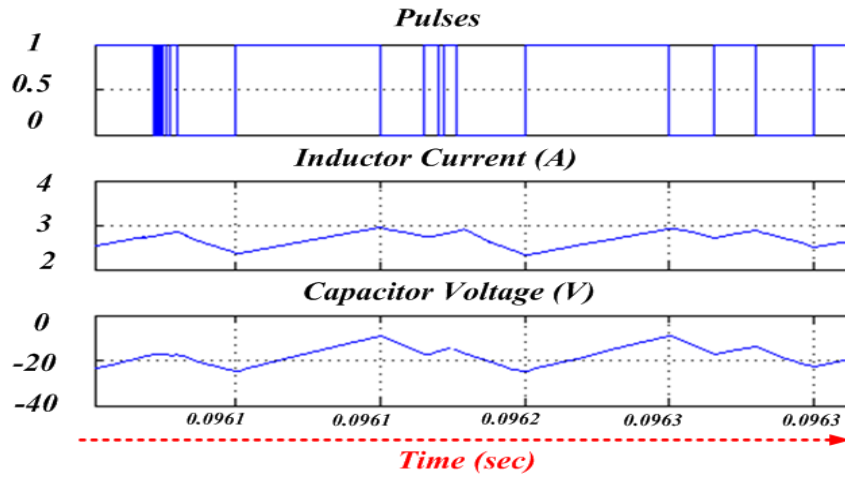


Figure 8. Inductor Current and capacitor voltage waveform with  $i_{ref}=2.85A$

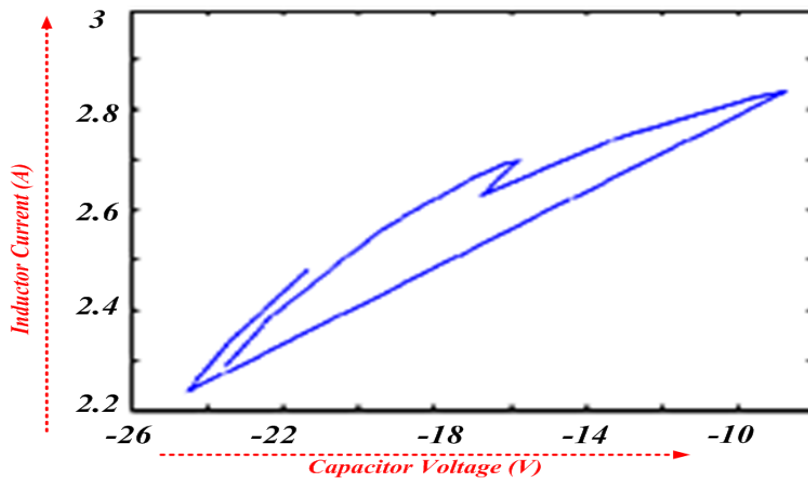


Figure 9. Phase Portrait of period 2 regime

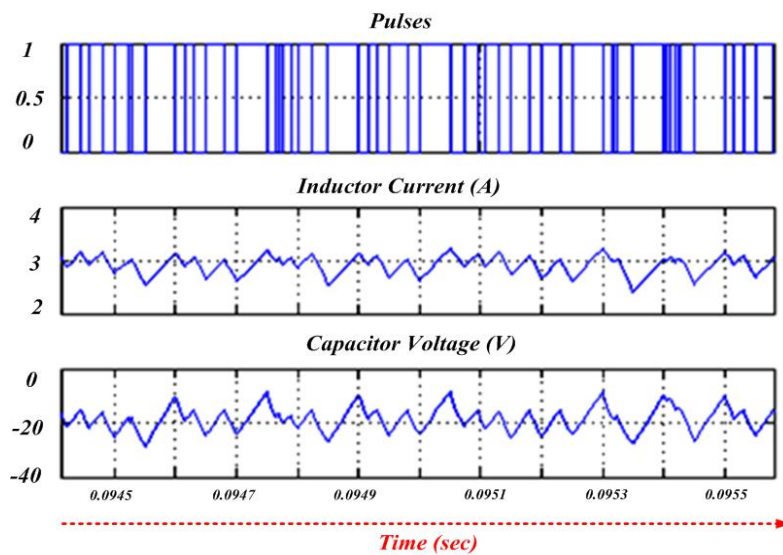


Figure 10. Inductor Current and capacitor voltage waveform with  $i_{ref}=3A$

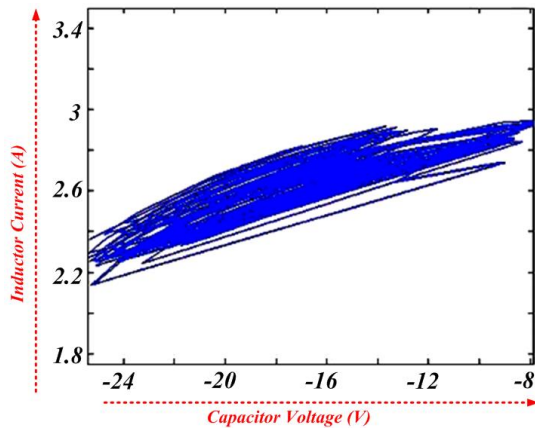


Figure 11. Phase Portait of chaotic regime

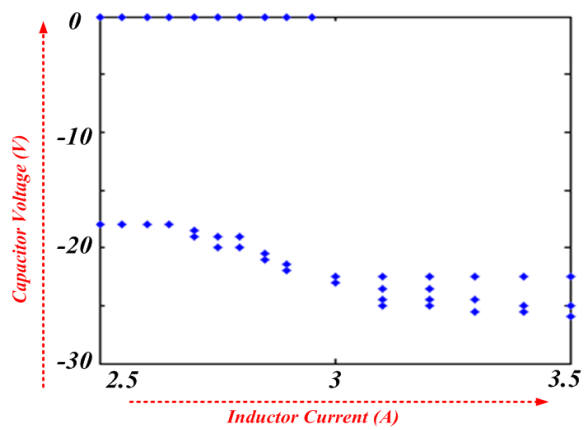


Figure 12. Bifurcation diagram between Iref and Vc

### 5. WEAK PERIODIC PERTURBATION METHOD OF CHAOS CONTROL[10-12]

To operate the system in the desired periodic regime, a small perturbation can be applied. By applying a small perturbation to a chaotic system, unstable periodic orbits will become stable [13-20]. This method of control is non-feedback control method. Figure 13. shows the Buck boost converter with weak periodic perturbation method of control. Any one of system parameter can be considered as control variable for controlling periodic perturbation, with the following form

$$x = (1-\eta)x + \eta(1 + \sin(2\pi ft)) \quad (14)$$

where,  $x$  represents the control variable

$\eta$  is the strength of controlling perturbation .

$\sin(2\pi ft)$  is the periodic perturbation signal

' $f$ ' is the frequency of the perturbation signal.

Without the weak periodic signal the converter experiences the non-periodic oscillations and also it leads to chaotic operation. When the weak periodic signal acts on the non-periodic signals and chaotic regimes, non periodic oscillations are broken. The chaotic control of current mode controlled buck boost converter using weak periodic perturbation control is simulated using the MATLAB/SIMULINK software [13-31]. The input voltage is kept fixed at 12V. Without any control, the converter operates in period-2 regime with  $I_{ref}=2.85A$  and in chaotic regime with  $I_{ref}=3A$ . With the same  $I_{ref}$ , converter operates in period -1 regime when WPP is applied. It is shown in Figure 14 and Figure 13 [13-20].

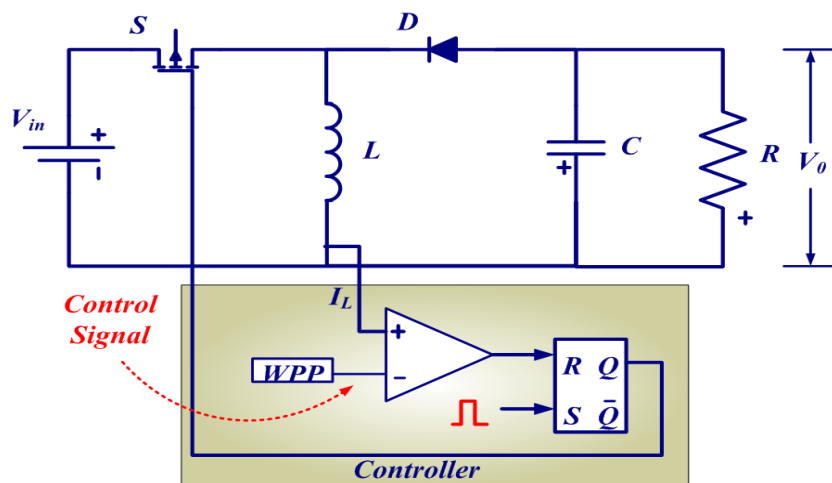


Figure 13. Buck-Boost Converter with weak periodic perturbation method of control



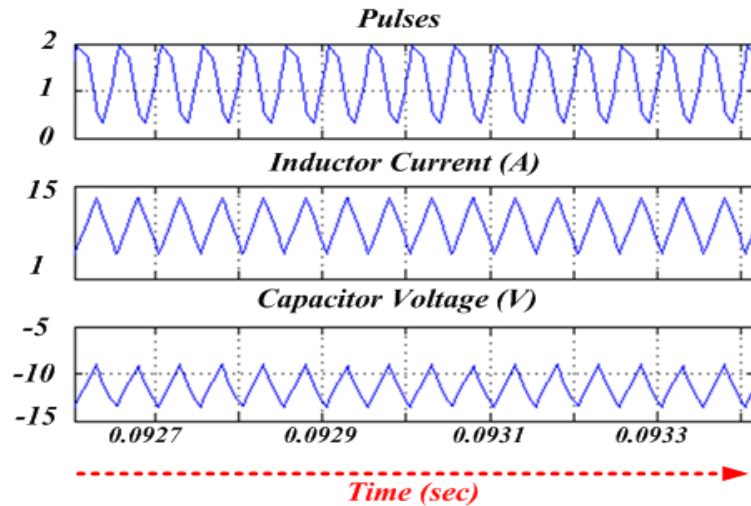


Figure 14. Controlled waveform of Inductor Current and capacitor voltage with  $i_{ref}=2.85A$

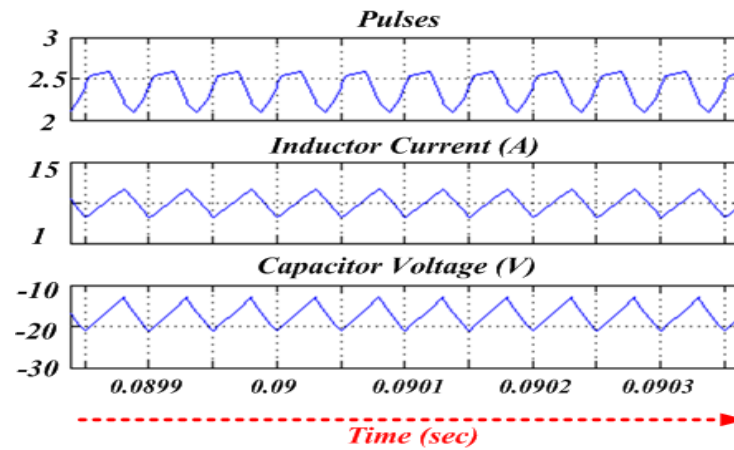


Figure 15. Controlled waveform of Inductor Current and capacitor voltage with  $i_{ref}=3A$

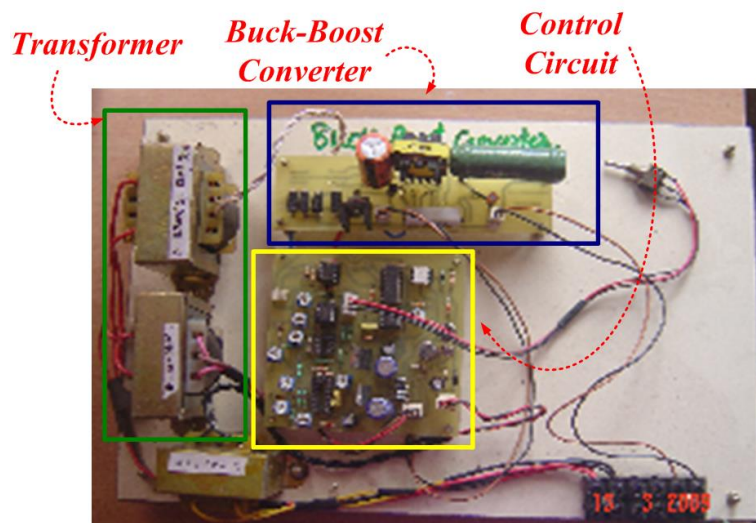


Figure 16. Hardware setup of current mode controlled buck boost converter

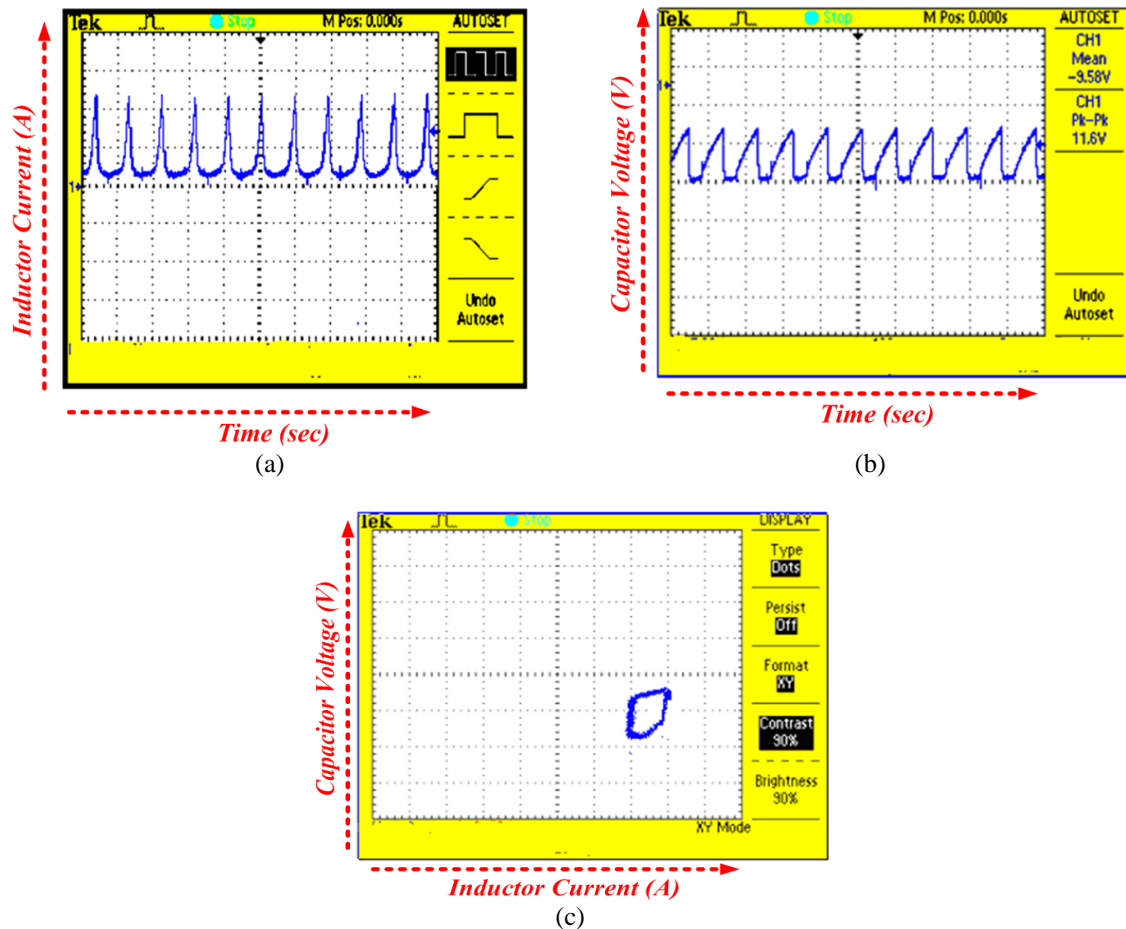


Figure 17. Waveforms during period-1 operation (a) Inductor current waveform of period -1 operation, (b) Capacitor voltage waveform of period -1 operation, (c) phase portrait of period-1 operation

## 6. HARDWARE IMPLEMENTATION OF CURRENT MODE CONTROLLED BUCK BOOST CONVERTER

The hardware implementation of buck-boost converter, including WPP method is shown in Figure 16. The supply voltage of 230V, 50Hz has been stepped down to 12V with the help of a step down transformer. A bridge rectifier rectifies ac voltage. After filtering through the capacitors, the required voltage of +5V for the control circuit was obtained using the regulator chip. The current mode controlled buck boost converter circuit is shown in the Figure 13. The converter is assumed to be operated in the continuous conduction mode [21-31].

The control circuit consists of comparator, flip-flop, buffer and a square wave generator, which are realized by analog and digital devices. The inductor current  $I_L$  is chosen as the programming variable which generates the on-off driving signal from the switch  $S$  after comparing it with the perturbed reference current  $I_{ref}$ . At the beginning of each cycle, the flip flop is 'set' by the timer, i.e., its output signal is high and the MOSFET IRF540 is ON. The output signal is low and the MOSFET is OFF when the flip flop is 'reset' by the output of the comparator. The resistor  $R$  is connected in series with the inductor, is used to compare the inductor current with the reference current  $I_{ref}$ .

Therefore the output of the comparator is high when the inductor current reaches the value of  $I_{ref}$ , whereas it is low when the inductor current is less than  $I_{ref}$ . The oscillator NE555 has been used for the generation of clock pulse for the flip flop HCF4013BE. Along with the proper resistor and capacitors, NE555 is used to produce the square wave pulse with the amplitude of 5V, a frequency of 20 KHz and duty cycle of 0.6. The IC LM8038 is used to generate the sine wave signal for the WPP control circuit and MCT2E is the opto coupler used to couple the control circuit with the driver circuit. The output from the flip flop turns the the MOSFET through the driver. The buck-boost converter dynamics are studied by varying the reference current [13-31].

The experimental results of inductor current, capacitor voltage and corresponding phase portrait of

period 1 regime are shown in the Figure18. When the reference current  $I_{ref}$  is further increased to 2.85A, the period doubling stage is reached. The experimental results of inductor current, capacitor voltage and the corresponding phase portrait in period 2 regime are shown in the Figure 18.

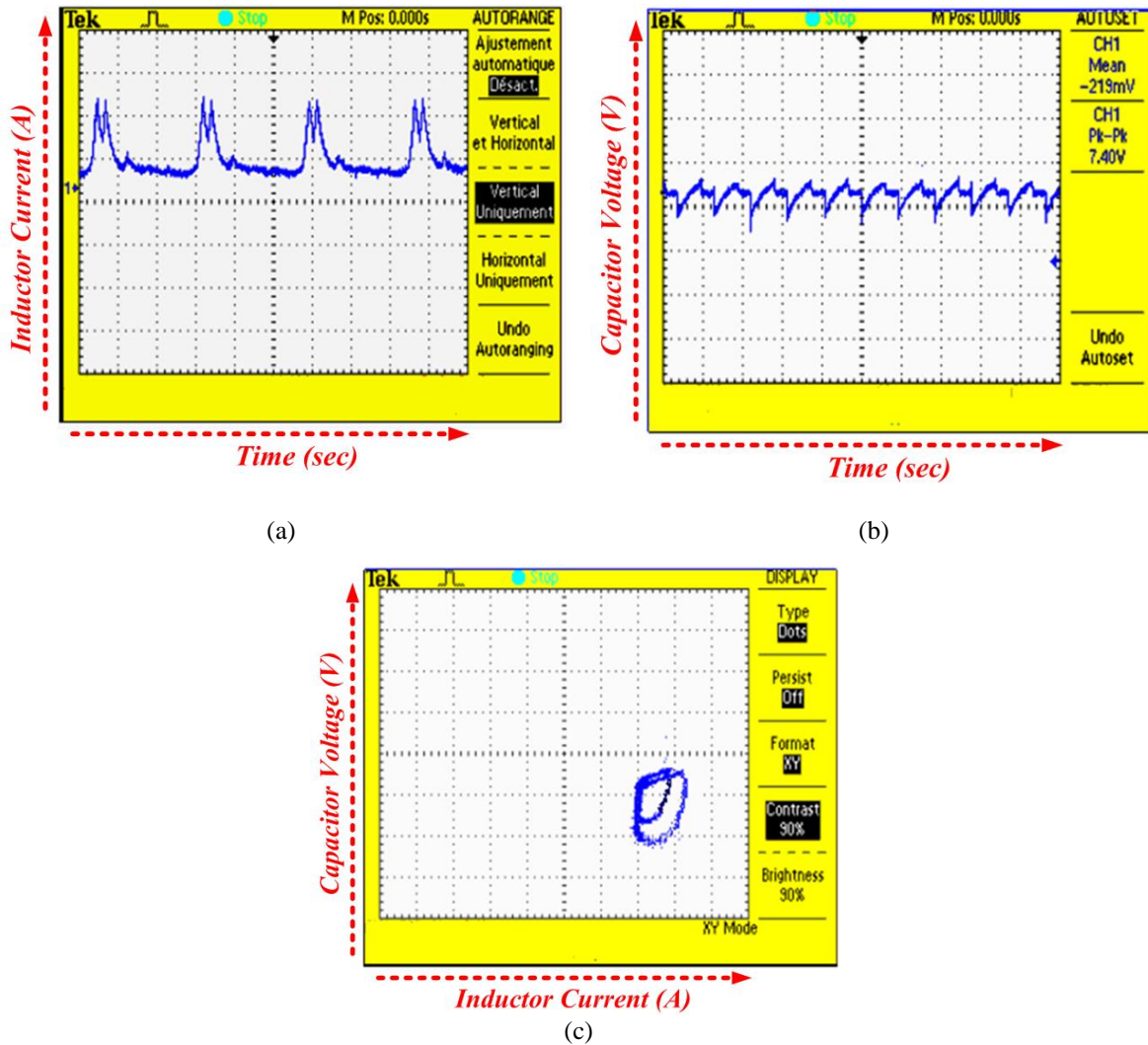


Figure 18. Waveforms during period-2 operation (a)Inductor current in period -2 regime, (b) Capacitor voltage in period -2 operation, (c) phase portrait of period-2 operation

## 7. CHAOS CONTROL USING WPP

The chaotic stage is obtained when reference current is raised to 3A. The experimental results of inductor current, capacitor voltage and phase portrait showing the chaotic operation are shown in the Figure 19. The inductor current and capacitor voltage and the corresponding phase portrait in the desired region is obtained by applying WPP are shown in the Figure 20 and Figure 21 respectively.

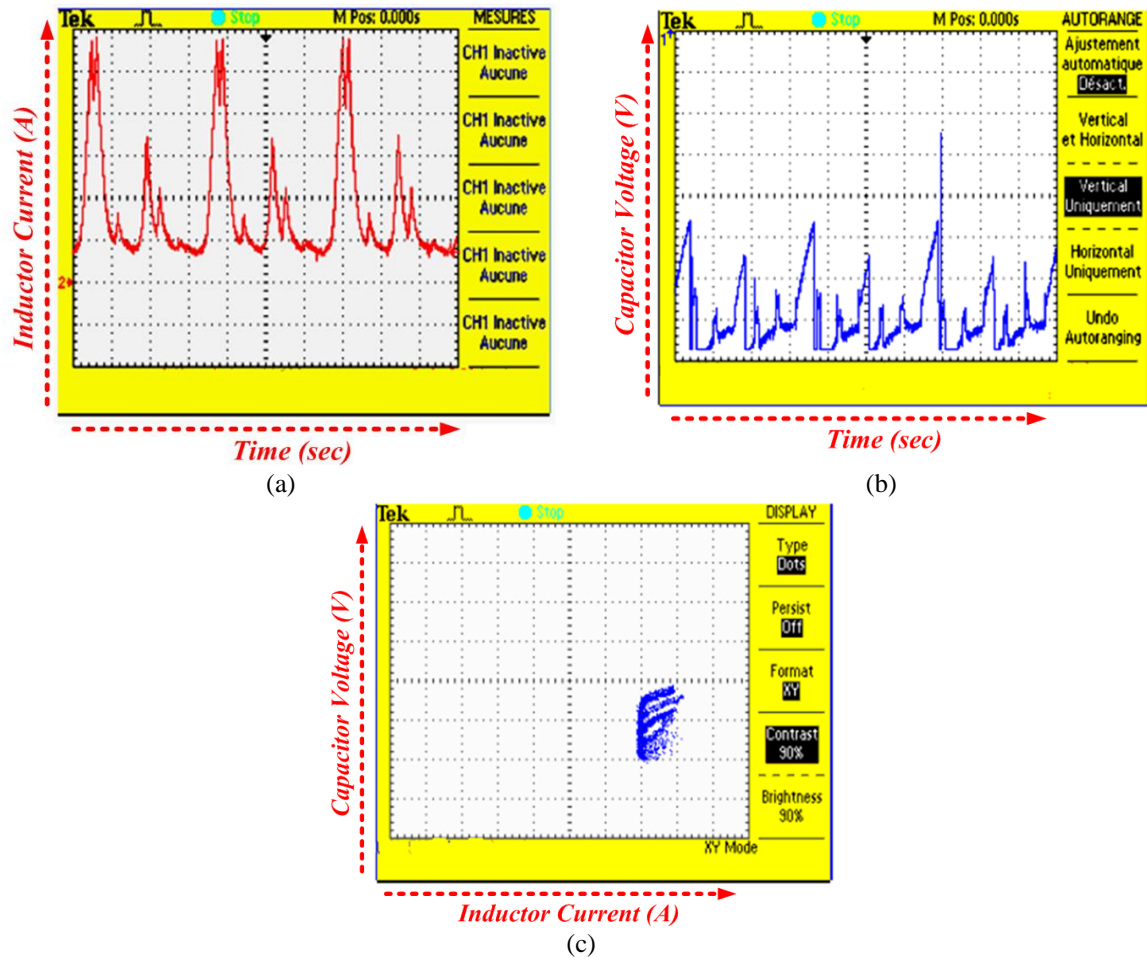


Figure 19. Waveforms during chaotic operation (a) Inductor current waveform of chaotic operation, (b) Capacitor voltage waveform of chaotic operation, (c) phase portrait of chaotic operation

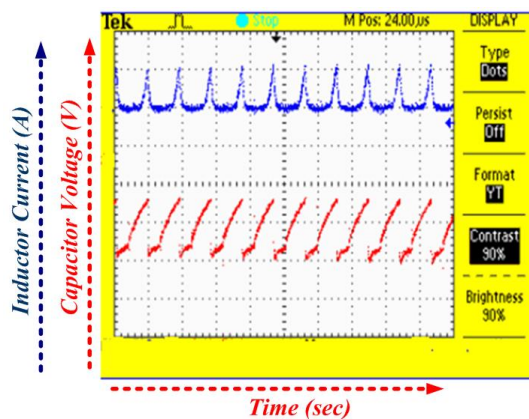


Figure 20. Controlled output voltage and current waveform

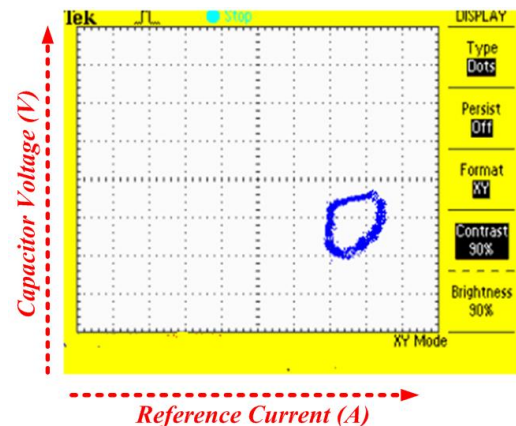


Figure 21. Controlled phase portrait

## 8. CONCLUSION

The chaotic behaviour of dc-dc current mode controlled buck boost converter is analysed. The simulated results of current controlled buck boost converter with weak periodic perturbation are obtained and presented using MATLAB. The bifurcation diagram is between reference current and input voltage with the inductor current as the reference. The results obtained reveal that the current mode controlled buck boost

converter shifts from periodic regime to chaotic regime when the reference current varied from 2.65A to 3A. The chaotic behaviour is controlled using weak periodic perturbation. It is also realized in hardware and the results are verified with the simulation results.

## REFERENCES

- [1] P.Balamurugan, A. Kavitha, P. Sanjeevikumar, J.L. Febin Daya, Tole Sutikno, "Periodic Perturbation Method for Controlling Chaos for a Positive Output DC-DC Luo Converter", Intl. Journal of Power Electronics and Drive Systems (IJPEDS), Institute of Advanced Engineering and Science (IAES) Publication, Indonesia, vol. 8, no. 2, pp. 775-784, Jun. 2017.
- [2] C.K.Tse and Mario di Bernardo, "Complex behavior in switching power converters", IEEE proceedings, Vol.90, No.5 May 2002, 768-771.
- [3] Ned Mohan and M.Undeland, "Power Electronics Converters, Application and Design", John Wiley and Sons, 1995.
- [4] Ilse Cevantes, IEEE member and Jose Alvarez-Ramirez "A Simple Chaos Control Strategy for DC-DC Power Converters" The 30th Annual Conference of the IEEE Industrial Electronics Society, November 2 - 6, 2004, Busan, Korea
- [5] G. Poddar, K. Chakrabarty, and S. Banerjee "Control of Chaos in DC-DC Converters" " IEEE transactions on circuits and systems-I: Fundamental theory and applications, Vol.45, NO 6, and June 1998.
- [6] Ka Wai Eric Cheng, Mingjian Liu, and Yiu Lun Ho "Experimental Confirmation of Frequency Correlation for Bifurcation in Current-Mode Controlled Buck-Boost Converters" IEEE power electronics letters, Vol 1, NO. 4, December 2003
- [7] Experimental study bifurcation and chaos in Buck-Boost converter, K.W.E. Cheng, M. Liu and J. Wu .\*/E€ Pro.-Eleirce: Powr Appt.. Vol 10, IW,. 1. Jmun. XU3
- [8] A.Gupta, S.Banerjee and D.Kastha "Experimental Study of Bifurcations in the Current Controlled dc-dc Buck-Boost Converter" National Conference on Nonlinear Systems & Dynamics, NCNSD-2003.
- [9] Rue-Ron Hsu, Han-Tzong Su, Jyh-Long Chern, and Chia-Chu Chen "Conditions to Control Chaotic Dynamics by Weak Periodic Perturbation", Vol 78, Number 15, Physical Review Letters.
- [10] M.di.Bernardo, L.Glielko, F.Vasca, Feb.1998, "Switching, bifurcations and chaos in dc-dc converter," IEEE Trans. Circuits Syst.-Part I, Vol.45, pp.133-141.
- [11] Z. Abbadi "Taming chaotic dynamics with weak periodic perturbations: an elucidation and critique". National Institute of Standards and Technology. Vol. 13, No. 2, 153-156, April 2002.
- [12] Wuyin Jin, Jianxue Xu, Ying Wu, Zhiyuan Rui. "Controlling neuronal spike by ion channels with weak periodic perturbation", Fifth World Congress on Intelligent Control and Automation (IEEE Cat.No.04EX788), 2004
- [13] M.S.Bhaskar, P.Sanjeevikumar, Frede Blaabjerg, "Multistage DC-DC Step-Up Self Balanced and Magnetic Component Free Converter for Photovoltaic Applications – Hardware Implementation", Energies Journal, MDPI AG Publications, Switzerland, vol. 10, no. 5, Issue 719, pp. 1–28, 18 May 2017.
- [14] C.Bharatiraja, S.Raghu, J.L Munda, P.Sanjeevikumar, "Analysis, Design and Investigation on a New Single-Phase Switched Quasi Z-Source Inverter for Photovoltaic Application", Intl. Journal of Power Electronics and Drive Systems (IJPEDS), Institute of Advanced Engineering and Science (IAES) Publication, Indonesia, vol. 8, no. 2, pp. 853-860, Jun. 2017.
- [15] P.Sanjeevikumar, G.Grandi, Frede Blaabjerg, Patrick Wheeler, Pierluigi Siano, Manel Hammami, "A Comprehensive Analysis and Hardware Implementation of Control Strategies for High Output Voltage DC-DC Boost Power Converter", International Journal of Computational Intelligence System (IJCIS), Atlantis Press and Taylor and Francis publications, vol. 10, no. 1, pp. 140–152, 2017.
- [16] P.Sanjeevikumar, Frede Blaabjerg, Patrick Wheeler, Joseph Olorunfemi Ojo, Ahmet H.Ertas, "High-Voltage DC-DC Converter Topology for PV Energy Utilization —Investigation and Implementation", Journal of Electric Power Components and Systems, Taylor and Francis publications, pp. 1–12, Dec. 2016.
- [17] P.Sanjeevikumar, Ersan Kabalci, Atif Iqbal, Haitham Abu-Rub, Olorunfemi Ojo, "Control Strategy and Hardware Implementation for DC-DC Boost Power Conversion Based on Proportional-Integral Compensator for High Voltage Application", Engineering Science and Technology: An International Journal (JESTECH). Elsevier Journal Publications, vol. 18, no. 2, pp.163–170, Jun. 2015.
- [18] P.Sanjeevikumar, K.Rajambal, G.Balaji, "Investigation of DC-DC converter topologies for future microprocessor", Asian Power Electronics Journal (APEJ) of Research, Power Electronic Research Centre, The Hong Kong Polytechnic University, Hung Hom, Hong Kong, vol. 2, no. 2, pp. 89–95, Oct. 2008. Digital ref: AI70301193. ISSN: 1995-1051.
- [19] P.Sanjeevikumar, K.Rajambal, "Extra high voltage DC-DC boost converters with simplified control strategy", International Journal of Modeling and Simulation, Hindawi Publishing Corporation, US, vol. 2008, Article ID 593042, 8 pages, Jan. 2008. ISSN: 1697-5591, EISSN: 1687-5605.
- [20] M.S.Bhaskar, P.Sanjeevikumar, Viliam Fedák, Frede Blaabjerg, Patrick Wheeler, "L-L Multilevel Boost Converter Topology For Renewable Energy Applications: A New Series Voltage Multiplier L-L Converter of XY Family", The 19th IEEE Intl. Conf. on Electrical Drives and Power Electronics, IEEE-EDPE'17, 4-6 Oct. 2017, Dubrovnik, Croatia (Europe). (Accepted for Publication).
- [21] M.S.Bhaskar, P.Sanjeevikumar, Pandav Kiran Maroti, Viliam Fedák, Frede Blaabjerg, Aishwarya Taur, "New 2LC-Y DC-DC Converter Topologies for High-Voltage/Low- Current Renewable Applications: New Members of X-Y



- Converter Family”, The 19th IEEE Intl. Conf. on Electrical Drives and Power Electronics, IEEE-EDPE’17, 4-6 Oct. 2017, Dubrovnik, Croatia (Europe). (Accepted for Publication).
- [22] T.Anuradha, P.Deiva Sundari, P.Sanjeevikumar, Pierluigi Siano, Zbigniew Leonowicz, “Comparative Analysis of Common MPPT Techniques for Solar PV System with Soft Switched, Interleaved Isolated Converter”, IEEE 1st Industrial and Commercial Power System Europe, 17th International Conf. on Environment and Electrical Engg., IEEE-I&CPS/IEEE-EEEIC’17, Jun. 6-9, 2017, Milan (Italy).
  - [23] M.S.Bhaskar, P.Sanjeevikumar, Frede Blaabjerg, Lars E.Norum, Ahmet H.Ertas, “4Nx Non-Isolated and Non-Inverting Hybrid Interleaved Boost Converter Based On VLSI Cell and Cockroft Walton Voltage Multiplier for Renewable Energy Applications”, Proc. of Intl. Conf. on Power Electron., Drives and Energy Systems, IEEE-PEDES’16, Kerala (India), 14-17 Dec. 2016.
  - [24] M.S.Bhaskar, P.Sanjeevikumar, Frede Blaabjerg, Rishi Kulkarni, Sridhar Seshagiri, Amin Hajizadeh, “Novel LY DC-DC Converter of XY Family with Minimal Internal Resistance Effect on Output Gain Ratio”, 4th IET Intl. Conf. on Clean Energy and Technology, IET-CEAT’16, Kuala Lumpur (Malaysia), 14-15 Nov. 2016.
  - [25] M.S.Bhaskar, P.Sanjeevikumar, Frede Blaabjerg, Olorunfemi Ojo, Sridhar Seshagiri, Rishi Kulkarni, “Inverting Nx and 2Nx Non-Isolated Multilevel Boost Converter For Renewable Energy Application”, 4th IET Intl. Conf. on Clean Energy and Technology, IET-CEAT’16, Kuala Lumpur (Malaysia), 14-15 Nov. 2016.
  - [26] 43. M.S.Bhaskar, P.Sanjeevikumar, Olorunfemi Ojo, Marco Rivera, R.Kulkarani, “Non-Isolated and Inverting Nx Multilevel Boost Converter For Photovoltaic DC Link Applications”, Proc. of IEEE Intl. Conf. on Automatica, XXII Congress of the Chilean Association of Automatic Control, IEEE-ICA/ACCA’16, University of Talca, Talca (Chile), 19-21 Oct. 2016.
  - [27] M.S. Bhaskar, P. Sanjeevikumar, Pat Wheeler, Frede Blaabjerg, Marco Rivera, Ahmet H.Ertas, R. Kulkarni, “X-Y Converter Family: A New Breed of Buck Boost Converter for High Step-up Renewable Energy Applications”, Proc. of IEEE Intl. Conf. on Automatica, XXII Congress of the Chilean Association of Automatic Control, IEEE-ICA/ACCA’16, University of Talca, Talca (Chile), 19-21 Oct. 2016.
  - [28] M.S.Bhaskar, P.Sanjeevikumar, Frede Blaabjerg, Viliam Fedák, Mihai Cernat, R.Kulkarani, “Non Isolated and Non-Inverting Cockcroft Walton Multiplier Based Hybrid 2Nx Interleaved Boost Converter For Renewable Energy Applications”, Conf. Proc. of The 17th IEEE Power Electronics and Motion Control, IEEE-PEMC’16, Varna (Bulgaria), 25-30 Sept. 2016.
  - [29] P.Sanjeevikumar, Frede Blaabjerg, Pierluigi Siano, Luigi Martirano, Zbigniew Leonowicz, Kiran M. Pandav, “PI and Fuzzy Control Strategies for High Voltage Output DC-DC Boost Power Converter – Hardware Implementation And Analysis”, Conf. Proc. of 16 IEEE Intl. Conf. on Environment and Electrical Engg., Florence (Italy), 7-10 Jun. 2016.
  - [30] P. Sanjeevikumar, G.Grandi, Patrick Wheeler, Frede Blaabjerg, J.Loncarski, “A Simple MPPT Algorithm for Novel PV Power Generation system by High Output Voltage DC-DC Boost Converter”, Conf. Proc., 24th IEEE International Symposium on Industrial Electronics, IEEE-ISIE’15, Rio de Janeiro (Brazil), pp. 214–220, 3–5 Jun. 2015.
  - [31] P.Sanjeevikumar, A.Iqbal, Haitham Abu-Rub, “Implementation and control of extra high voltage dc-dc boost converter”, The 7th IET International Conference on Sustainable Energy and Intelligent System, IET-SEISCON’13, Chennai (India), pp. 182–188, 12–14 Dec. 2013.